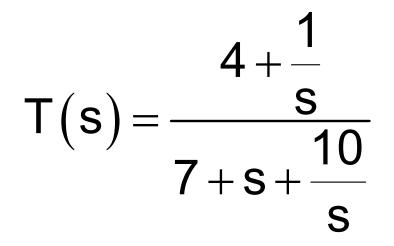
# EE 230 Lecture 6

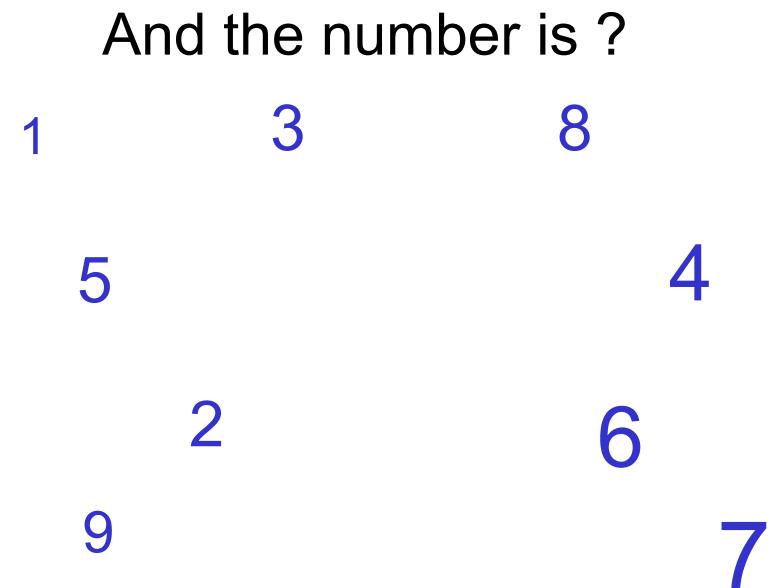
#### **Linear Systems**

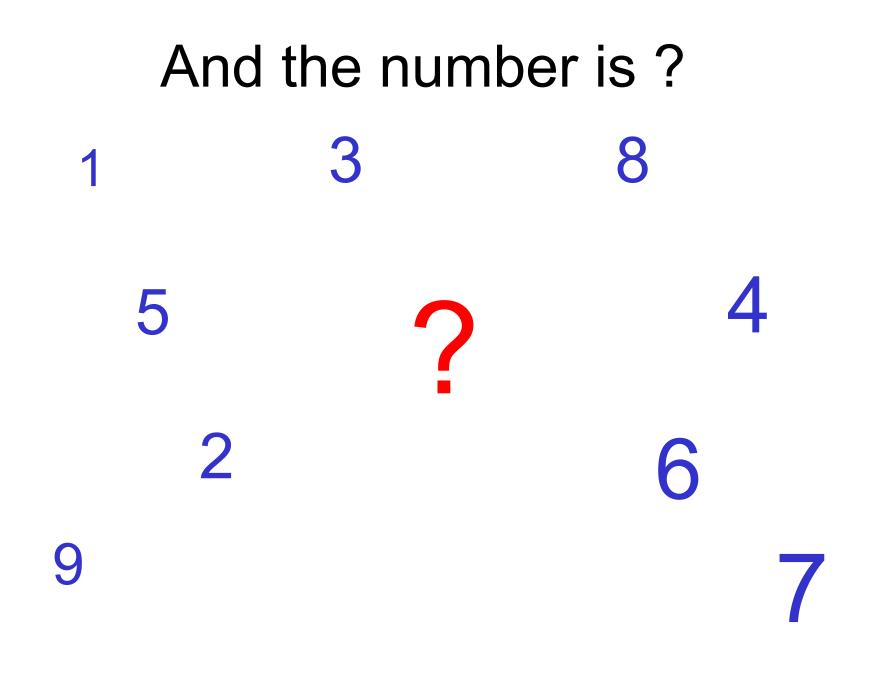
- Poles/Zeros/Stability
- Stability

# Quiz 5

A system has the transfer function T(s) Determine the poles of the system.







# Quiz 5 A system has the transfer function T(s) Determine the poles of the system.

$$T(s) = \frac{4 + \frac{1}{s}}{7 + s + \frac{10}{s}}$$

Solution:

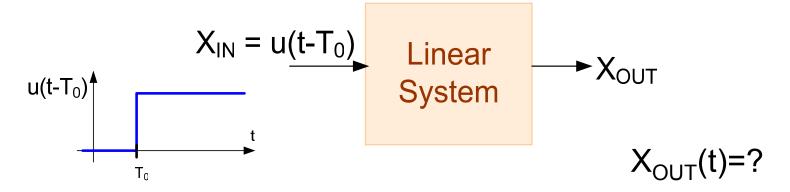
$$T(s) = \frac{4 + \frac{1}{s}}{7 + s + \frac{10}{s}} = \frac{4\left(s + \frac{1}{4}\right)}{s^2 + 7s + 10}$$
$$T(s) = \frac{4\left(s + \frac{1}{4}\right)}{s^2 + 7s + 10} = \frac{4\left(s + \frac{1}{4}\right)}{(s + 2)(s + 5)}$$

Poles at s = -2 and s = -5

#### Review from Last Time Step Response of First-Order Networks



Many times interested in the step response of a linear system when the system is first-order

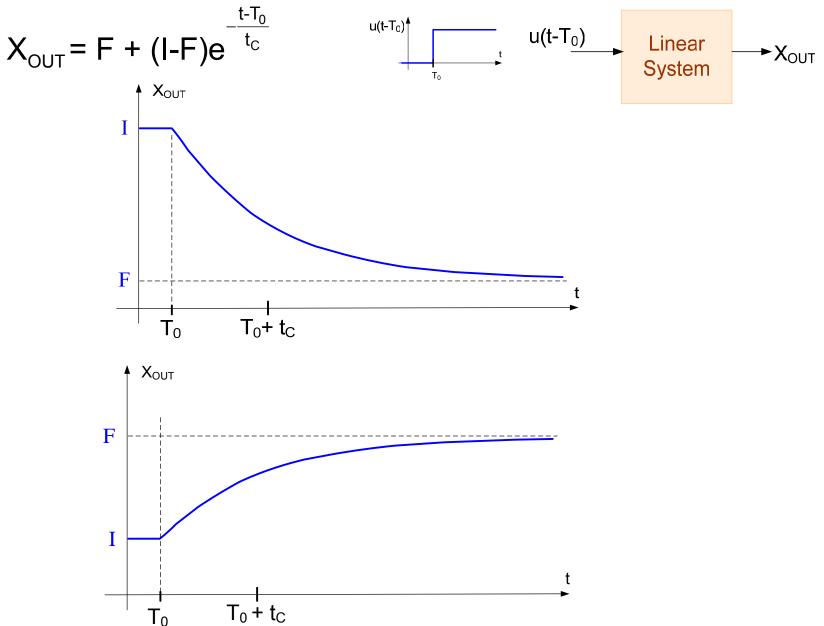


For any first-order linear system, the unit step response is given by

$$X_{OUT} = F + (I-F)e^{-\frac{t-1}{t_{c}}}$$

I is the intital value, F is the final value and  $t_{\rm C}$  is the time constant

#### Review from Last Time Step Response of First-Order Networks



#### Review from Last Time Step Response of First-Order Networks

Example:

Obtain the step response of the circuit shown if the step is applied at time T=1msec and prior to  $V_{OUT}(t)=0$  for t<1msec. Assume R=1K, C=0.1uF

Solution:

$$T(s) = \frac{1}{1 + RCs}$$
$$T(s) = \frac{\frac{1}{RC}}{\frac{1}{1 + RCs}}$$

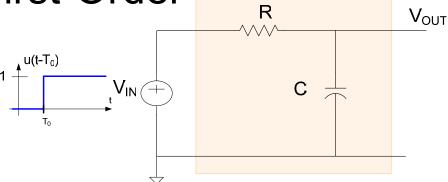
s+ <sup>1</sup>/<sub>RC</sub>

This is first order and of the form:

$$T(s) = \frac{\kappa}{s-p}$$
  $\therefore p = -\frac{1}{RC}$   $t_c = -p^{-1} = RC$ 

Thus, the output can be expressed as:

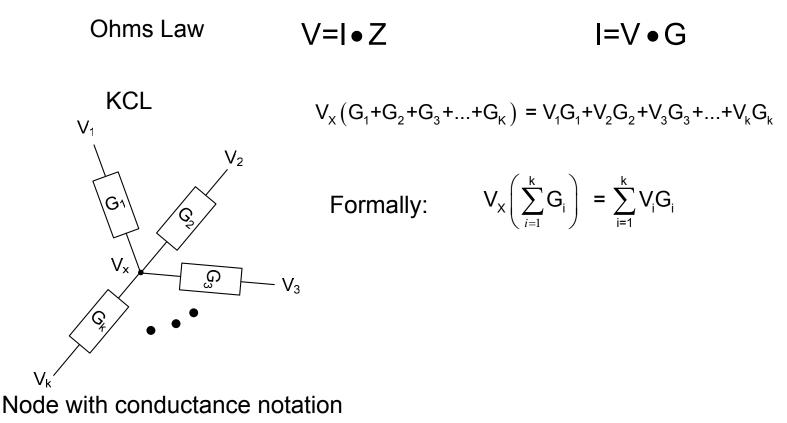
$$V_{OUT} = F + (I-F)e^{-\frac{t-T_0}{t_c}}$$



F=1V  
I=1V  
$$V_{OUT} = 1 + (-1)e^{-\frac{t-.001}{RC}}$$
  
 $V_{OUT} = 1 - e^{-\frac{t-.001}{RC}}$ 

#### Review from Last Time Impedance and Conductance Notation

Circuit Analysis with Impedance Notation (Z) and Conductance Notation (G)



KCL is often the fastest way to analyze electronic circuits

Why?

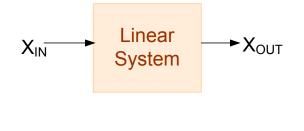
Conductance notation is often much less cumbersome than impedance notation when analyzing electronic circuits Why?

**Review from Last Time** 

#### Poles and Zeros of Linear Networks

For any linear system, T(s) can be expressed as

 $T(s) = \frac{\sum_{i=0}^{n} a_i s^i}{\sum_{i=0}^{n} b_i s^i}$ 



where  $a^{}_i$  and  $b^{}_i$  are all real,  $b^{}_n \ \neq \ 0$  ,  $a^{}_m \ \neq \ 0$  , and  $n \ge m$ 

Can always make b<sub>n</sub>=1

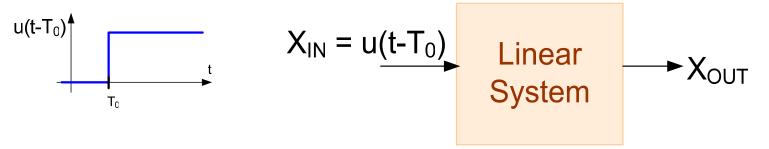
Numerator often termed N(s) Denominator often termed D(s)

$$T(s) = \frac{\sum_{i=0}^{m} a_i s^i}{\sum_{i=0}^{n} b_i s^i} = \frac{N(s)}{D(s)}$$

Definition: The roots of D(s) are the poles of T(s) and the roots of N(s) are the zeros of T(s)

The poles of T(s) are often termed the poles of the system

#### Step Response of First-Order Networks

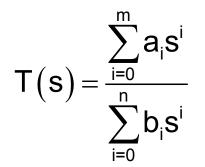


Claim: A system with a  $1^{st}$  order lowpass transfer function with a pole p and a dc gain K has a unit step response of

$$X_{OUT} = K + (I-K)e^{p(t-T_0)}$$

where I is the initial value of the output

$$T(s) = \frac{-Kp}{s-p}$$





Alternate representation of transfer function

$$\mathsf{T}(\mathsf{s}) = \mathsf{K} \frac{\prod_{i=1}^{\mathsf{m}} (\mathsf{s} - \mathsf{z}_i)}{\prod_{i=1}^{\mathsf{n}} (\mathsf{s} - \mathsf{p}_i)}$$

where  $K = \frac{a_m}{b_n}$  { $z_1, ..., z_m$ } are the poles and { $p_1, ..., p_n$ } are the zeros

#### **Response of Linear Networks**

If  $X_{IN}(s)$  is the input (in the s-domain) to a linear system, then the output (in the s-domain) is given by

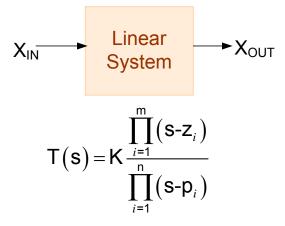
$$X_{out}(s) = T(s)X_{IN}(s)$$

$$X_{OUT}(s) = K \frac{\prod_{i=1}^{m} (s - z_i)}{\prod_{i=1}^{n} (s - p_i)} X_{IN}(s)$$

The Laplace transform of the excitation can be written as

$$\mathbf{X}_{\mathsf{IN}}(\mathbf{s}) = \mathbf{H} \frac{\prod_{i=1}^{\mathsf{r}} (\mathbf{s} - \alpha_i)}{\prod_{i=1}^{\mathsf{q}} (\mathbf{s} - \beta_i)}$$

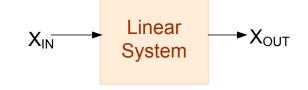
$$X_{OUT}(s) = KH \frac{\prod_{i=1}^{m} (s-z_i)}{\prod_{i=1}^{n} (s-p_i)} \bullet \frac{\prod_{i=1}^{r} (s-\alpha_i)}{\prod_{i=1}^{q} (s-\beta_i)}$$



#### **Response of Linear Networks**

If  $X_{IN}(s)$  is the input (in the s-domain) to a linear system, then the output (in the s-domain) is given by

$$X_{OUT}(s) = KH \frac{\prod_{i=1}^{m} (s-z_i)}{\prod_{i=1}^{n} (s-p_i)} \bullet \frac{\prod_{i=1}^{r} (s-\alpha_i)}{\prod_{i=1}^{q} (s-\beta_i)}$$



If the denominator terms are all unique, this can be expanded in a partial fraction as

$$X_{OUT}(s) = \left(\frac{\theta_1}{s - p_1} + \frac{\theta_2}{s - p_2} + \dots + \frac{\theta_n}{s - p_n}\right) + \left(\frac{\gamma_1}{s - \beta_1} + \frac{\gamma_2}{s - \beta_2} + \dots + \frac{\gamma_m}{s - \beta_m}\right)$$

The time-domain output can be obtained from the inverse Laplace transform as:

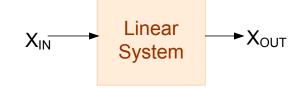
$$X_{OUT}^{-1}(s) = \left(\theta_{1}e^{p_{1}t} + \theta_{2}e^{p_{2}t} + \dots + \theta_{n}e^{p_{n}t}\right) + \left(\gamma_{1}e^{\beta_{1}t} + \gamma_{2}e^{\beta_{2}t} + \dots + \gamma_{m}e^{\beta_{m}t}\right)$$

The term in the left parenthesis is the natural response due to the network The term in the right parenthesis is the forced response due to the excitation

#### **Response of Linear Networks**

If  $X_{IN}(s)$  is the input (in the s-domain) to a linear system, then the output (in the s-domain) is given by

$$X_{OUT}(s) = KH \frac{\prod_{i=1}^{m} (s-z_i)}{\prod_{i=1}^{n} (s-p_i)} \bullet \frac{\prod_{i=1}^{r} (s-\alpha_i)}{\prod_{i=1}^{n} (s-\beta_i)}$$



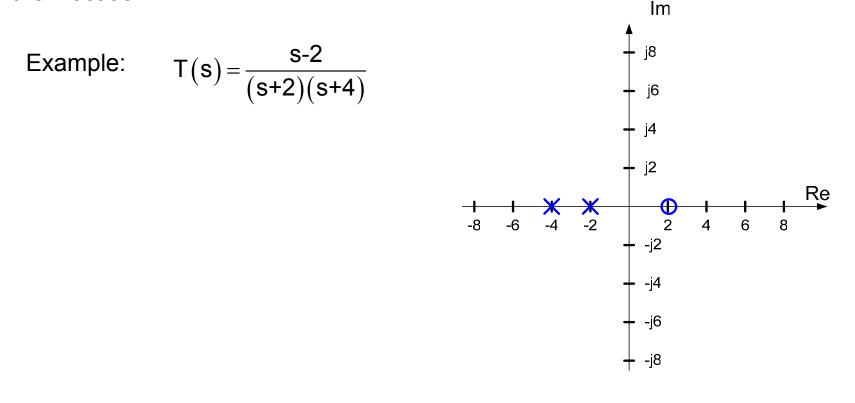
$$X_{OUT}^{-1}(s) = \left(\theta_{1}e^{p_{1}t} + \theta_{2}e^{p_{2}t} + \dots + \theta_{n}e^{p_{n}t}\right) + \left(\gamma_{1}e^{\beta_{1}t} + \gamma_{2}e^{\beta_{2}t} + \dots + \gamma_{m}e^{\beta_{m}t}\right)$$

If the real part of the poles are negative, the natural response will decay out but if the real part of the poles are positive, it will grow without bound !

The forced response will have properties that are similar to those of the excitation

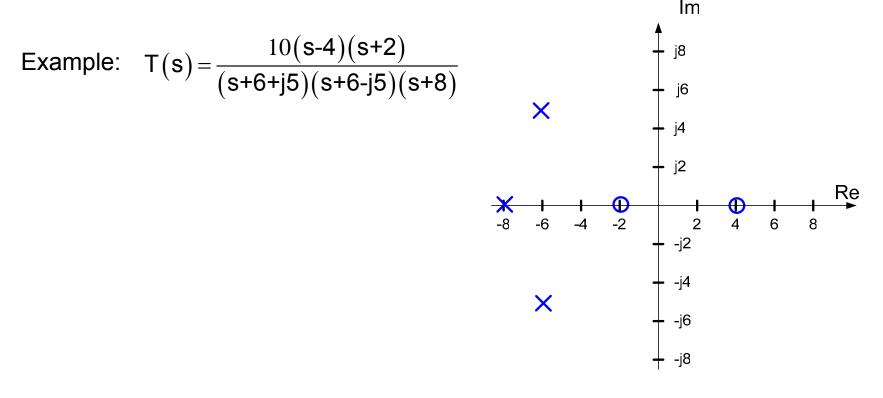


A plot of the poles and zeros in the complex plane is often used to visually show their location





A plot of the poles and zeros in the complex plane is often used to visually show their location



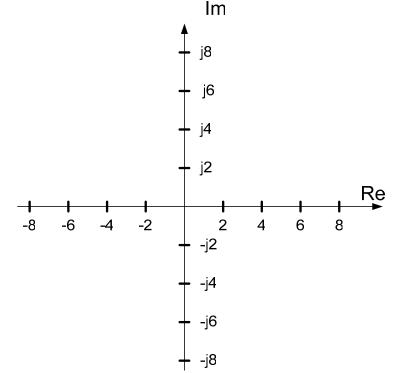


A plot of the poles and zeros in the complex plane is often used to visually show their location

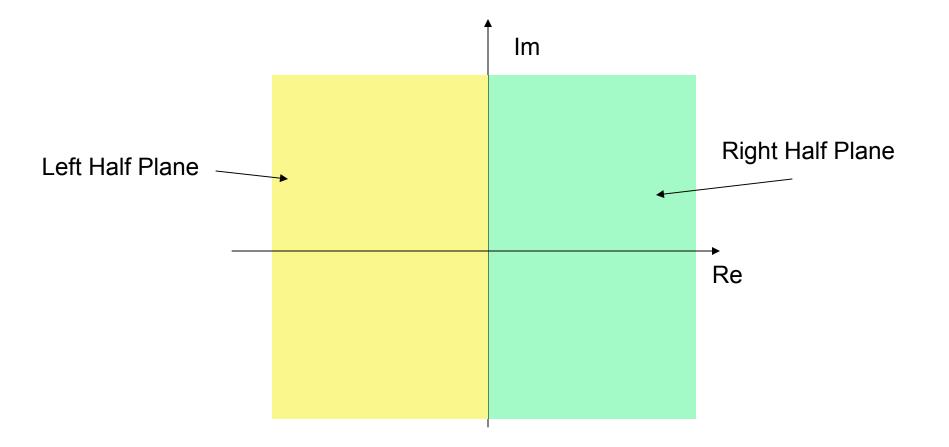
Example: 
$$T(s) = \frac{4s+1}{s^5 + s^4 + 2s^3 + 3s^2 + 2s + 1}$$
  
Zero as s=-1/4

Poles?

Numerical techniques must be used, closed form expression does not exist for polynomials of order 5 or higher

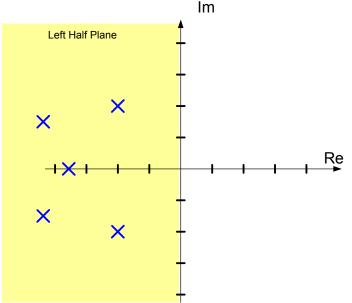


#### The Complex Plane

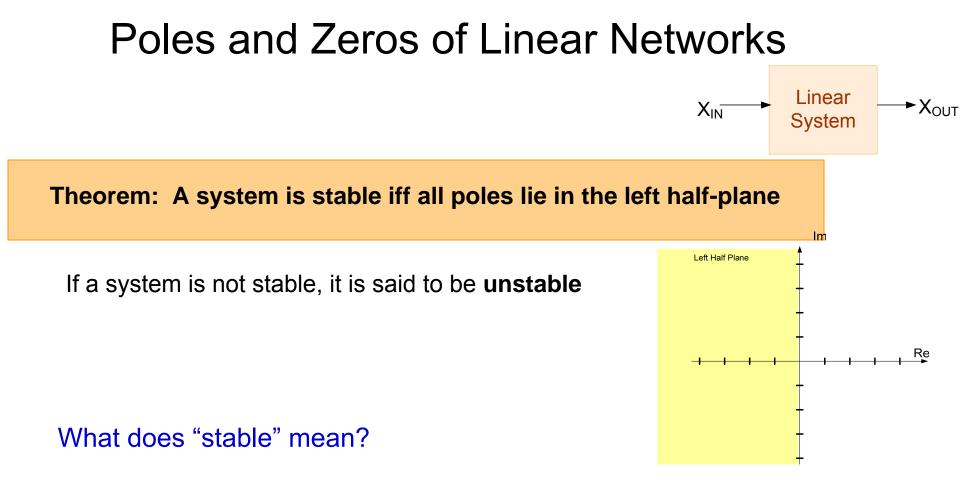




Theorem: Any network comprised of resistors, capacitors, and inductors will have all poles in the Left Half of the s-plane



Note: This theorem is not true in the more general case where the circuit may contain amplifiers or dependent sources



A linear system is stable iff <u>any</u> bounded input will result in a bounded output

A system is stable iff the output due to any appropriately small input does not cause the output to diverge to  $\pm \infty$  and does not create a time varying output that persists indefinitely



An unstable system will have one or more poles outside of the left half-plane

If a linear system is unstable, practically one of three things will happen a) A peridic output of constant amplitude will persist for ever

- b) A time-varying output will grow in amplitude with time
- c) The output will grow without bound towards  $+\infty$  or  $-\infty$

Practically, if a system is unstable, as amplitudes grow nonlinearities will be introduced and these nonlinearities will limit the growth of the output

Example: Determine if the following systems are stable

 $T(s) = \frac{1}{s+1}$  single pole at p= -1 ∴ system is stable

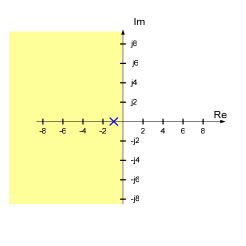
Step response (at t=0) if I=0

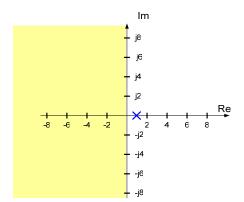
Since I=0 and F=1  $X_{OUT} = F + (I-F)e^{pt}$   $X_{OUT} = 1-e^{-t}$ 

T(s)=
$$\frac{1}{s-1}$$
 single pole at p= 1  
∴ system is not stable

Can be shown that step response (at t=0) if I=0 is  $X_{OUT} = 1 - e^{t}$ 

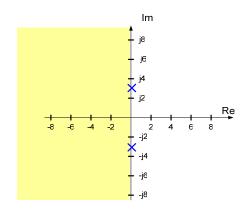
This diverges to -∞ as t increases !





Example: Determine if the following systems are stable

T(s)= $\frac{4}{s^2+9}$  poles at p= -3j and p=+3j ∴ system is not stable

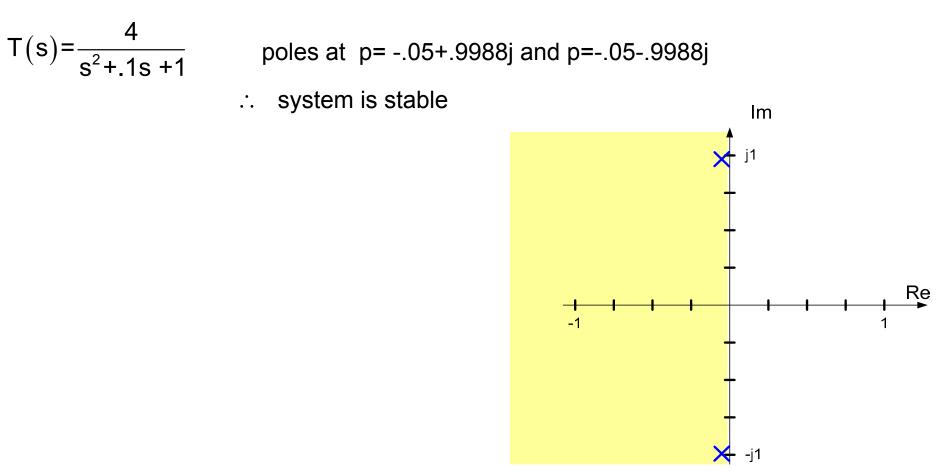


It can be shown that the step response will include a term

r(t) = Hsin3t

This is a time-varying input that persists indefinitely !

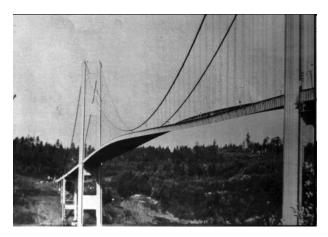
Example: Determine if the following systems are stable



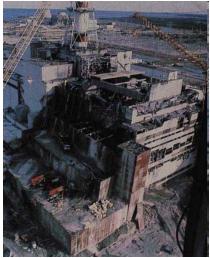
But since poles are so close to imaginary axis, natural response may ring for a while

#### Is stability good or bad?

#### Some unstable systems



Tacoma Narrows Bridge



Chernobyl

#### Is stability good or bad?

Some more unstable systems



HP 200A



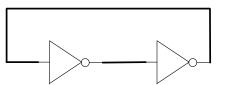
Flagship product that got Hewlett Packard started

#### Is stability good or bad?

Some more unstable systems



B1 Bomber (Stealth)





Taipei 101 (hopefully stable)

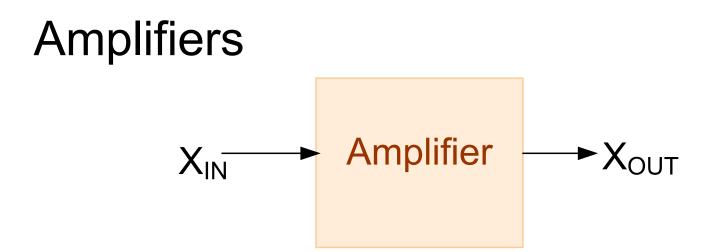
#### Is stability good or bad?

It depends upon what is desired

Many times instability is very undesirable

But often instability is very desirable as well

But regardless, it is almost always necessary to know whether a system is stable or unstable !



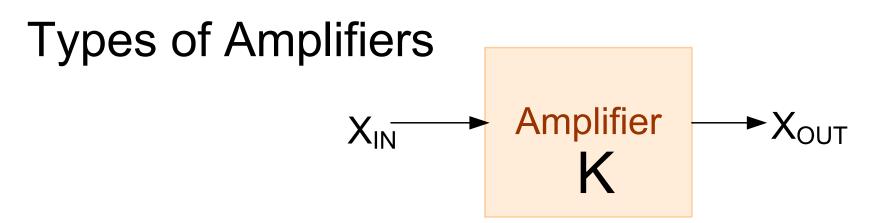
An ideal amplifier is linear and has a frequency independent transfer function that does not change with source or load impedance

Ideally, 
$$X_{OUT} = KX_{IN}$$

K is termed the amplifier gain

K=T(s)

Often K ">" 1 (when  $X_{IN}$  an  $X_{OUT}$  of same dimensions)



Assuming input and output variables from { I, V }

Input	Output	Туре	Dimensions
V	V	Voltage	Dimensionless
Ι		Current	Dimensionless
V		Transconductance	A/V (mho)
	V	Transresistance	V/A (Ω)

# **Types of Amplifiers**

Input	Output	Туре	Dimensions
V	V	Voltage	Dimensionless
I	I	Current	Dimensionless
V		Transconductance	A/V (mho)
I	V	Transresistance	V/A (Ω)

Why are there so many types of amplifiers?

- Because we can have them?
- Some transducers have ouput variables different than what is needed at output Sometimes performance can be optimized by using a particular amplifier type

Will show later that if amplifiers are not ideal, they all have the same model and differ only in the parameters in the model

# End of Lecture 6